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*Marketta Tehikoski*

Marketta Tehikoski  
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Osoite: Arkadiankatu 6 A Puhelin: 09 6939 500  
P.O.Box 1160 Telephone: + 358 9 6939 500  
FIN-00101 Helsinki, FINLAND

Telefax: 09 6939 5328  
Telefax: + 358 9 6939 5328

## A method for forming a film

5 The present invention relates to a method for forming a film on a planar surface, a device for forming a film on a planar surface, a method in rebuilding a converting line comprising means for forming a film on a surface of a sheet-like substrate and a multilayer sheet-like product comprising a film layer. The term planar surface means in this application either a surface of a sheet-like substrate or a counter surface on which surface the film is formed and peeled off after forming. In other words, the latter product is a film without the substrate. The sheet-like substrate means that the substrate is of a sheet material, for example paper, polymeric film or metal film. The substrate can be either in a sheeted form or as a continuous web, preferably it is as a continuous web. The counter surface can be for example an endless belt on which surface the film is formed.

20 The known methods for forming a film include processes for forming a continuous film web, such as the extrusion process, or processes for forming a film on a sheet-like substrate, such as suspension coating, solvent-base coating and extrusion coating (and lamination). The suspension coating can be used for production of barrier coatings and intermediate layers for wet and dry lamination. In spread coating the coat weight (or applied amount) is adjusted on the web by doctoring, and by roll application the coat weight can be adjusted prior to the application (e.g. gravure applicator). The web requires drying afterwards.

30 Wet lamination, in which water-based suspensions with dry contents of 40-50 % are mostly used, can be utilized to produce laminates such as aluminium foil/adhesive/paper or plastic film/adhesive/paper. Typical adhesives are casein, sodium silicate, starch, and latex (PVAc+EVAc, SB, PE or acrylates).

35 In dry lamination the water-based adhesive suspension is pre-dried on the web and then laminated with heat. Typically used polymers are

hardening (curable) polyurethanes, PVDC, modified SB and acrylic copolymers.

5 Important properties of polymer dispersion films are barrier properties, for instance the film shall not permeate water or steam, odour, taste, grease, fat, oil, gases such as oxygen, light, or radiation, such as UV radiation. Other required properties may be that it shall be printable, durable against rubbing, puncture and chemicals, and heat sealable. The polymer dispersion films are used for different packages  
10 (food/non-food) and wrappings (paper wrappings, bags and kraft paper sacks).

Solvent-base coating can also be used for preparation of wet and dry laminated webs. The process requires solvent evaporation, recovery  
15 and recirculation.

The solvent acts as a plasticizer within the polymer during drying, which will change the polymer crystal structure, often weakening its barrier properties. Additionally, there is a risk for residual solvent in the product. Solvent-base coating is used especially for PVDC-based  
20 copolymers and restrictedly for coating plastic films, e.g. PET.

The extrusion process involves melting and application of a thin polymer film onto the substrate or between webs. Multilayer application  
25 and double-sided coating are possible. The layer thickness produced at a time is approx. 5 – 100 µm.

The most common coatings are PE-LD, acid-modified copolymers, or polyethylene blends with thermosets or ionomers. Ionomers are  
30 especially used on metal surfaces.

Important properties of extrusion coated products are adhesion to the substrates, odor and taste, pinhole-free structure, no curling, barrier properties, heat sealability and coefficient of friction. The extrusion  
35 coated films are used in liquid packaging, other rigid packaging (folding cartons, cup boards, ovable boards), Industrial applications (wrapping for paper reels and sawn timber, reel end discs, ream



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- impermeable structure and good coverage of the film is achieved even by low amounts of the applied material,
- low amount of waste,
- flexibility of the processing line, substrates and the materials of the film,
- modified surface properties are easily achieved,
- the same system can be used for different materials with a small grade change time,
- no waiting or aging time before using the produced material as in the solventless lamination process,
- the rate and degree of polymer crystallization can be modified, and
- the production efficiency of the dry surface treatment process is up to 1200 m/min (the maximum speed of the methods of the prior art: the off-line extrusion 600 – 800 m/min, the spread coating 800 m/min)

Advantages of the dry surface treatment over the conventional extrusion process can be found both in the fields of technical solutions and material handling. The same powder deposition unit suits for application of a variety of powders of different source and for manufacture of various products. Possibly changes of the supply systems and application geometries are necessary but the material-specific dies or screws are avoided such as required in extrusion. Through the air-borne powder supply, even hard and coarse pigment particles can be added in, which in extrusion might cause wearing of the screw section, and are used only in limited amounts. Then also specially optimised production variables are required (e.g. line speed). The overall maintenance work is low, because the powder-formed materials can be changed relatively fast without extensive control adjustments in the conversion operations. In extrusion the screw requires cleaning operations, i.e. purging with a low-viscosity polymer when cooling down or changing the material.

Advantages over extrusion include the short duration of melt processing. Also complex flow channels are avoided. In extrusion, due to the longer melt period, the material can suffer from temperature

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differences causing changes in the melt fluidity, possibly material solidification or polymer degradation and therefore problems in pumpability. Temperature differences can also impair interlayer adhesion in coextrusion. In a fast thermomechanical treatment the  
5 deforming polymer is not drawn or stretched as extensively as in extrusion (lower shear rates in the nip), so the stress relaxation-related problems afterwards are lesser. In the sintered products the low residual stress restricts the post-treatment shrinkage. In comparison,  
10 the resulting polymer film drawn at the extruder die is very material-specific and can therefore have irregularities such as uneven thickness profile (neck-in), melt fracture (the melt sticks to the die) and problems in adhesion (control of oxidation in the air gap). In coextrusion, the different viscosities of the layers can cause problems by interflow, unevenness and thickness variations.

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Advantage over solvent-based coatings is that there will be no residual solvents in the product, especially when the materials are chosen so that there are none or only low content of volatile plasticizers that are released during healing. High efficiency of the process relates to the  
20 low amounts of waste during start-up and conversion operations and low extent of edge cutting. There are possibilities for material recovery and recycling, as the excess powder can be removed before fixation. Also the risk of entrapped air in the laminate is low after the fixation nip(s).

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Since the process consists of the application, fixing and surface modification steps without intermediate drying or preliminary melting, the converting unit is very compact. In addition, the manufacture of multilayer structures simplifies, because no special equipments  
30 (coextrusion die) or extra extruders or application units are needed. On the contrary to the dry surface treatment process, drying capacity and recovering systems are energy-intensive and require large-scale investments in processes of the prior art.

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The dry surface treatment process is environmentally safe. An eliminated water or solvent usage in the surface treatment process combined with more gentle melt processing are the main environment-

related advantages. The reduction of energy consumption can also be achieved since the evaporation step is eliminated and no after-drying section is needed.

- 5 The dry surface treatment process of different substrates comprises the dry powder application followed by thermomechanical fixing in at least one heated roll nip. The coated and laminated products can be composed of layers of paper or board, plastic films, metal foils or metallized films, treated either one or double-sided with the dry surface treatment process. The application of the powdery film forming material
- 10 utilises an electric field to transfer the particles to the substrate surface to form a granular layer and to enable an electrostatic adhesion prior to the thermal treatment. Both the final adhesion and the surface smoothening/texturing or lamination within two substrates is executed
- 15 simultaneously through thermomechanical treatment in a heated roll nip by melting the granular layer formed of the powdery film forming material.

- 20 A continuous development toward more compact surface treatment processes leads toward simultaneous treatment of both sides of the substrate and total on-line surface treatment. The dry surface treatment process provides additional possibilities to make the converting process even more compact by omitting the wetting-drying-cycles, solvent evaporation or melt processing encountered in conventional
- 25 processes. The application and smoothening or lamination steps are integrated into one single process. Such a change provides possibilities to reduce both investment and production costs (e.g. overall efficiency, raw material and energy). It will also require changes in preparation and handling of the coating and adhesive raw materials.

- 30 The dry surface treatment process also adds possibilities to explore new converting product properties. This is achieved as a result of an eliminated rewetting of the base paper surface related to the suspension coating applications and shortened melt processing times
- 35 related to the extrusion applications. The coating powder also stays on the substrate surface and e.g. with low coat weights ( $2 - 8 \text{ g/m}^2$ ) almost perfectly covers the surface without possibilities to penetrate or adsorb

into the structure. A distinct interface between the film layer and the substrate can be observed in the cross-section of a dry-formed product.

- 5 The applied polymer can also be treated to form porous non-uniform layer, favoured for example in some printing applications. The available materials could be e.g. inorganic and plastic pigments or highly absorptive polymers. There are possibilities for matte, glossy, transparent, coloured and pigmented polymer-based surfaces and connecting layers. Inorganic pigments may be used as additives or to give extra value, e.g. if a more porous surface is favourable.

- 15 When producing the powdery film forming material for the dry surface treatment process, the materials can be prepared directly via the polymerization process or precipitation from suspension, and possibly refining by e.g. grinding. When preparing multicomponent powders, the components are combined or prepared separately either as dispersions in a liquid phase (e.g. water etc.), prior to entering an evaporation or drying process, in a gas phase (e.g. air etc.), or in a melt-mixing phase prior to granulation and grinding, as shown in table 1. Therefore, there are several methods available to produce, refine and combine the coating components.

- 25 Polymer materials applicable in powder form include thermoplastics such as polyamides (PA: Nylon-11 and Nylon-12, preferably high crystalline grades), polyolefins like polyethylene (PE-LD, PE-LLD, PE-HD, PE-MD), polypropylene (PP), and their copolymers, polyesters like poly(ethylene terephthalate) (PET) and poly(butylene terephthalate) (PBT), and others like poly(vinylidene chloride) PVDC, poly(tetrafluoroethylene) (PTFE), polyacetal (POM), ethylene-vinyl alcohol (EVOH), polyvinyl alcohol (PVOH), ethylene-vinyl acetate (EVA), polyvinyl butyral (PVB), acid copolymers, starch, ionomers, a selection of biodegradable polymers, and amorphous polymers like polystyrene (PS), acrylonitrile-butadiene-styrene (ABS), polyvinyl acetate (PVAc), polycarbonate (PC), poly(methyl methacrylate) (PMMA) and polyvinyl chloride (PVC) can be used. Available thermosetting polymers are e.g. epoxies and its blends, formaldehydes



and some polyesters. Grinding of sticky (low Tg) plastics may require cryogenic conditions.

5 The inorganic pigments include e.g. ground calcium carbonate, precipitated calcium carbonate, kaolin, calcined clay, talc, titanium dioxide, gypsum, alumina trihydrate and silica pigments. The amount of inorganic material in the powdery film forming material is 40 wt-% at the most, preferably 20 wt-% at the most and more preferably 12 wt-% at the most. It is possible that there is no inorganic material, and in  
10 some films manufactured according to the method of the invention it is advantageous if the granular layer is free from inorganic material. The mentioned possibilities of producing the powdery film forming material are summarised in table 1.

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Table 1. Description of the possibilities for manufacturing and blending of the components of the powdery film forming material.

Polymerisation process	Dispersion medium	Physical state
High-pressure polymerisation	Gas	Mechanical mixture of separate inorganic pigment and polymer particles
		Blend particles of inorganic pigment and polymer(s) ground to powder
Polymerisation in supercritical conditions	Gas	Separate inorganic pigment and polymer(s)
		Hybrid of inorganic pigment with polymer(s)
Suspension polymerisation	Liquid	Separate inorganic pigment and polymer(s) particles
		Hybrid particles of inorganic pigment and polymer(s)

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The formation of a uniform film layer requires powder melting, spreading and adhesion on the substrate surface. These are affected by e.g. thermal and pressure conditions, initial particle size, rheological properties of the melt, substrate roughness and chemical compositions (i.e. surface energies, bonding sites, multicomponent materials). When the materials require some kind of refining, the preparation process parameters require optimisation to create a fine-sized and homogeneous powdery film forming material without forming strong aggregates in the dried or ground powder. These aggregates could due to their large size give an uneven and too porous film layer interfering the permeation properties. Polymer thermal deformability during thermomechanical treatment determines the layer properties such as density, openness, smoothness, strength and optical properties.

The particle properties directly influence the conditions during the initial powder application, which includes the fluidised bed during powder transport and electrostatic deposition as an initial adhesion. By grinding mm-scale polymer granulate particles, particles in the range 50-250  $\mu\text{m}$  have been produced. Also the drying conditions of the material blends in suspensions have been found to greatly influence the particle size distribution of the coating powder. Aggregates in the range 5-500  $\mu\text{m}$  after spray drying and 1-100  $\mu\text{m}$  after freeze-drying have been produced. The average aggregate or particle size can be further reduced when applying a certain post-grinding. Favourable particle size does not exceed 100  $\mu\text{m}$ , but particles as small as a few nm can be used. It can be said that a particle size close to 10  $\mu\text{m}$  would be preferable in respect to the charging properties but it depends on the powdery film forming material. The components of the powdery film forming material can have varying electrical properties such as particle surface charging and discharging rate.

A considerable reduction of the applied polymer amounts has been possible due to further optimised thermomechanical fixing conditions (e.g. dwell-time, surface temperature and linear load). Barrier coatings and adhesive layers produced by the dry surface treatment process can have an advantage from the lowest possible film weights. The applicable film weight in one application is 3 - 60  $\text{g/m}^2$ , which

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corresponds to approx. 3 – 100  $\mu\text{m}$  layer thickness with plastics. Powder fineness allows the application of thin film layers, and the formed layer homogenize with a feasibly low energy input in the thermomechanical treatment compared to that in the extruder mixing section.

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It is advantageous if all the steps of the manufacturing process are made in dry conditions. For example, the powder components should be produced as dry or the preparation needs to be done in another carrier medium than water (e.g. air, another gas or an evaporable liquid). This is to be done to avoid the related costs and possible powder defects such as too strong agglomeration and large particle size.

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The most profitable way could be preparation of dry powder components without the need for drying where the particle morphology is adjusted in the production process. Fine-sized polymeric particles can also be formed by synthesis in a gas phase, for example in supercritical carbon dioxide ( $\text{sc-CO}_2$ ). The separation of the solvent from product is simplified because  $\text{CO}_2$  reverts to the gaseous state upon depressurisation, thus eliminating energy intensive drying steps. The selection of suitable monomers is quite large, including combinations of styrene, butadiene, vinyls, acrylates, and olefinic monomers (typically emulsion, suspension, or bulk polymerized grades). The end product is a dry powder with a particle size between 0.2 and 10  $\mu\text{m}$  readily recovered by venting  $\text{CO}_2$ .

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In dry surface treatment process of miscellaneous converting substrates, the powdery film forming material for forming the granular layer is sprayed through an area of strong electric field and high free-ion concentration to the surface of the substrate. The powdery film forming material is put into the feeder chamber and transferred to the powder deposition unit with compressed air. The compressed air is used for many purposes such as powder fluidizing, transporting, and conditioning. As the complexity of the application equipment, the charging unit and the powdery film forming material properties vary, the importance of a continuous supply of clean and dry air also

Increases. The air quality (e.g. temperature and moisture variations) and powder piping can generate contaminants in the compressed air, which may cause process and quality problems. The contaminants in the compressed air can also consist of vapour, liquid or solids.

5

The powdery film forming material is charged in the powder deposition unit. A primary requirement for electrostatic powder deposition is generation of large quantities of gas ions for charging the aerosol particles. This is accomplished by means of a gaseous discharge or corona-treatment. The generation of a corona involves the acceleration of electrons to high velocity by an electric field. These electrons possess sufficient energy to release an electron from the outer electron shell when striking neutral gas molecules, thus producing a positive ion and an electron. This avalanche phenomenon is initiated around the discharge or corona electrode.

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An electric field is created by the voltage application to the electrode pair. The electric field in the interelectrode space has three main purposes: (1) a high electric field near the electrode with a small radius of curvature leads to the generation of charging ions in an electrical corona, (2) the field provides the force that causes these ions to collide with and transfer their charge to the particles of the powdery film forming material, and (3) it establishes the necessary force to attach the charged particles of the powdery film forming material to paper. If the small radius electrode is negative (e.g. negative corona), electrons from the corona region move toward the grounded (e.g. positive) electrode and the positive ions move toward the negative electrode. To achieve a reversed polarity (positive corona), the positive ions move toward the grounded electrode and the electrons move toward the positive electrode with a small radius.

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Instead of one-sided application of the powdery film forming material, also a two-sided application is possible. The two-sided application comprises a negative and positive corona used at the same time. As the electrode is negative (negative corona region), the electrons in the negative corona region move towards the positive electrode (positive corona) and the positive ions towards the negative electrode. On the

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opposite side of the substrate (positive corona region), the positive ions move towards the negative electrode and the electrons towards the positive electrode.

- 5 In the case of an excess supply of the powdery film forming material, the electrostatic deposition can also be utilised to remove it. The uncharged or charged powder excess, which floats in the deposition unit can be charged with secondary electrodes. Then the powder collection can be done for example through electrostatic precipitation or  
10 air suction.

The powdery film forming material can be precharged with triboelectric charging, corona charging, or charged in situ. Precharging strengthens the impact of the electric field on the powder.

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- The powdery film forming material is supplied to the application unit with compressed air or another transport medium that promotes particle charge. The transport medium can be added to the supply air e.g. through oxygen addition or entirely replace the supply air by  
20 another gas. Also the moisture content and the temperature of the supply air can be varied to improve the charging effect in the corona region. This might further improve the powder transfer in the electric field to the substrate surface. A higher temperature of the supply air increases the ionisation coefficient. The supply air temperature should  
25 not influence the properties of the powdery film forming material, it should not exceed the polymer glass transition or melt temperature ( $T_{air} < T_g, T_m$  of the polymer) and result in powder agglomeration. The moisture content of the supply medium is to be kept below a relative humidity (RH) of 50 % to avoid discharges and raise the medium  
30 pressure beyond 0.1 bar. This decreases the amount of harmful discharge. The powder stream can be parallel or directed perpendicular to the web. The parallel powder stream can also be used to overcome the air boundary layer. As the powder is accelerated to the same velocity as the web, the electrostatic forces may be used to  
35 pull the web and the particles together. The powder deposition can also be made by using a dielectric belt and an electric field. In a multilayer deposition, the powder components are deposited separately or as

powder blends. The grounding electrode geometry can then be either a platy stationary electrode or a circular rotating electrode (o.g. operating as a belt or as a roll).

- 5 Voltage and current are varied with the required distance between the charging and the grounding electrodes, the material properties (o.g. dielectric constants) of the electrodes, the powder composition (resistivity, dielectric constants of the powder etc.), the powder amount, the supply medium moisture content and pressure. The voltage varies from 5 kV to 1000 kV and the current from 30  $\mu$ A to 1000 A. The powder properties and the application concept (one-sided or two-sided) guides set-up of the charging electrodes. The charging electrodes are however either positive or negative.
- 10
- 15 Another possibility to charge the particles of the powdery film forming material is to use a system producing triboelectric charges. The particles are charged in contact with another material, and the strength of charging is adjusted e.g. by materials contacting each other, or the time the materials are in contact with each other. The triboelectric charging depends strongly on the properties of the contacting materials, and it can be evaluated for example by utilizing suggestive triboelectric series. The surface properties of the powdery film forming material can, however, be modified in different ways, for example by forming a thin surface layer on the particles of the film forming material.
- 20
- 25 This can effectively be used to change the triboelectrification properties of the material.

It is also possible to combine both corona charging electrodes and a system for producing triboelectric charges in a same device.

- 30 Instead of the sheet-like substrate on which surface a granular layer is formed, a substantially planar surface can be used. The planar surface is a part of the film forming machine, such as an endless belt. A granular layer is formed on the belt, the granular layer is finished to form a film, and the film is peeled off from the belt after cooling the film. The film may be orientated by a suitable manner, for example by
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stretching. Such a film forming process can be used for example instead of the extrusion process.

5 After forming the granular layer on the surface of the substrate, the granular layer is finished to form a film. The finished film is substantially free from pinholes. The powder melting and fixing is accomplished in a thermomechanical treatment with an optimal combination of temperature (80–350 °C), linear load (15–450 kN/m) and dwell time (0.1–1000 ms; speed 150–1200 m/min; nip length 3–1000 mm). The reinforced fixation can be used in different ways to achieve desired properties. The thermomechanical treatment can be made by conventional calendering methods or calendering-like methods. The conventional calendering methods include hard-nip, soft-nip, long-nip (e.g. shoe-press), condebelt and super-calendering. One of the most essential parts in the thermomechanical fixing is the non-adhesive property of the contacting roll surfaces to avoid blocking, sticking or other build-up of polymer based deposits. When powders with a low polymer content (< 20 pph) are used, hard metal or PTFE-based roll cover materials are suitable. When powders with a high polymer content (>20 pph) are used, the roll cover must have better non-sticking properties, e.g. usage of PTFE-based covers is preferred.

25 It is possible to chill the film after the thermomechanical finishing stop. The chilling rate of the dry surface treated product can be controlled, so the rate and degree of polymer crystallization can be modified. This affects e.g. the barrier properties.

30 In some cases, the increased surface moisture content of the substrate improves the powder deposition and fixing on the surface. An incoming substrate moisture content (e.g. hydrophilic film bulk moisture) can be adjusted to optimise the layer strength and other product properties. For example, starch requires a higher moisture content than hydrophobic polymers to reach equivalent binding strengths. This can be explained by the need to solubilise the starch to improve deformability and give binding properties but then an excess energy is required for water evaporation. The surface moisture can also be adjusted through nozzle application onto the substrate surface. Then

only a water amount evaporating in the fixing process is applied and the moisture balance over the fixing stage remains constant. The nozzle application can be done before the powder application or the thermomechanical fixing.

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Several applied layers and double-sided coatings can be produced on the same line. In multilayer application of powders the separation of layers is maintained due to the electric repulsive forces. The preceding layer can, but does not have to be fixed before applying the next. To ensure adhesion between the applied layers, some degree of interlayer diffusion should occur during fixation.

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Low processing temperatures are possible due to the mechanical load in the nip(s). Therefore the range of processable materials broadens into more temperature-sensitive grades and high molecular weight polymers. High molecular weight polymers have improved mechanical properties but often problems in processability due to their rheological character. Shorter melt processing reduces the risk of over-oxidation, found harmful e.g. in heat sealing.

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In conventional extrusion the layer thickness is controlled by the screw speed (output rate), die gap, draw ratio and linear load of the chilling nip. Profile control in dry surface treatment (both in the machine direction and the cross direction) will be simplified and possibly quickened by electrostatic application. In multilayer application, not all the layers have to be the same width. There is a possibility to form bands of the powdery film forming material, advantageous for example in converting products to be sealed. Another possibility to utilize the partial film layer is to form bands from a material, which reacts to different gaseous substances for example by changing its colour. When such a layer is an inner layer of a packaging material, the layer will react for example to oxygen penetrating inside the package after it is damaged or a layer can be reactive with the overlying printing ink indicating a broken structure when the two materials are in contact. The above-mentioned layer can also be between the layers forming the packaging material but then it is advantageous if the film is substantially continuous.



There are various uses for the films produced by the dry surface treatment process. Polymer-based film layers have a wide variety of functions. Impermeable structures are formed by so-called barrier coatings and barrier sealing layers. Different materials work as barriers for liquids, vapours, gases and light (e.g. water, steam, oxygen, flavours and oils). Typically a combination of materials gives the best result and often one material has several functions. The successive layers must be chosen so that the overall structure acts as a two-way barrier (prevents leakage or permeation from the outside to the inside or vice versa). The layer must be free from pinholes, compositional and physical irregularities and possess good adhesion to the substrate layer. Connective layers of adhesives are used to form the bonding layer between webs in extrusion lamination or in a separate process (e.g. dry lamination).

Specified heat sealing materials are used in converting products to be folded or/and seamed to different shapes. In some applications the seam must be peelable. Low sealing temperature and high hot-tack (strong adhesion as a melt) of the adhesive are favourable for less energy-intensive and fast sealing operation. Polymer-based coatings are used for mechanically improved protective surfaces, over-print lacquering and surface waxing. For example, polyethylene based waxes are suitable for use in the process of the invention. They provide protection against mechanical loads, improved lubrication and appearance. In addition, metal surfaces may require a sealing layer to prevent oxidation.

Often the converting process includes also printing. Depending on the printing process, the substrate meets the requirements of e.g. absorption (porosity), and resistance against abrasion, moisture, solvents and heat. In some applications the surface requires an over-print protective coating.

Required mechanical properties of a coated or laminated product include e.g. bending strength (no delamination or cracking), abrasion and impact resistance and durability of the barrier properties under

mechanical and environmental loading with the passage of time. For some applications the optical and electrical properties of the products should be able to modify.

- 5 The method of the invention is suitable for forming e.g. food packaging products. Characteristic properties of the packaging products are a low oxygen transmission rate and a low water vapour transmission rate. According to DIN 3985, the oxygen transmission rate is generally at the most 180 ml/m<sup>2</sup>/24 h (23°C, RH 0%), and the water vapour  
10 transmission rate is generally at the most 2,5 g/m<sup>2</sup>/24 h.

- Many products produced according to the present invention comprise the following layers: A printing layer on the reverse side of the plastic layer, an adhesive layer to attach successive layers to each other, and  
15 a metal layer composed of a metal foil or a metal coating on a plastic or paper layer.

- The prerequisite for forming the granular layer from the powdery film forming material is a continuous substrate onto the granular layer can  
20 be formed. One of the layers forming the final product acts as a basic material, and the other layers can be formed on it. The basic material needs not to be the outer or inner layer of the packaging material but it can also be some interlayer. The two-sided process is advantageous when films are formed on the both surfaces of the basic material. It is  
25 possible that even the basic material have been formed in a previous process step by the dry surface treatment process.

- In the following, the dry surface treatment process will be described by examples and a drawing in which the principal of the utilization of the  
30 one-sided dry surface treatment process is shown.

- A sheet-like substrate is unwound from a reel 1. An electric field 4 is formed between a negative electrode comprising a feeding nozzle 3 and a grounding electrode 8. To attain an even electric field, extra  
35 negative electrodes 2 are placed in the same row with the electrode by the feeding nozzle 3 to strengthen the performance of the electrode 3.

A grounding electrode 8 is on the reverse side (compared to the negative electrodes) of the substrate to be treated. The substrate is preferably in a continuous form. The grounding electrode 8 can be a stationary plate, or it can be a rotating roll. The rotating roll is  
 5 advantageous because the stationary plate tends to create uneven granular layers.

Air is led to the process by a compressor 7. A powdery film forming material is conveyed through a fluidised bed 6 and through a valve 5 to  
 10 the negative electrode comprising the feeding nozzle 3. Charged particles of the powdery film forming material are blown from the feeding nozzle towards the substrate. The particles form a granular layer on the substrate which is finished in the next process step.

15 The substrate is led to a nip formed between two counter rolls 9, 10. The roll 10 may be a resilient roll and the roll 10 may be a hard heated roll. The granular layer is melted in the nip to form an even substantially impermeable film. A ready product is wound to the reel  
 20 11.

Example.

Several alternatives for packaging materials are listed below. The alternatives are represented as there are made by the conventional  
 25 technique and layers which are possible to be formed by the dry surface treatment technique are marked with \*. Depending on the chosen basic material, also other possibilities for forming a layer by the dry surface treatment process may exist.

30 1. Caps or lids for e.g. pet food packaging:

- a polyester layer
- a printing layer
- an adhesive layer ( PE, PP, Surlyn)\*
- 35 - a metal coating or a metal layer
- a polyethylene layer\*

2. A packaging material for wafers is composed of the following layers:

- 5
- a polyester layer
  - a printing layer
  - an adhesive layer \*
  - a metal coating or a metal layer
  - co-extruded oriented polypropylene layer \*

10 3. A packaging material for snacks or Pommes frites is composed of the following layers:

- 15
- co-extruded oriented polypropylene layer
  - a printing layer
  - an adhesive layer \*
  - a metal coating or a metal layer
  - co-extruded oriented polypropylene layer \*

20 4. A packaging material for snacks and biscuits is composed of the following layers:

- 25
- a release layer \*
  - an orientated polypropylene layer
  - an adhesive layer \*
  - a printing layer
  - a metal coating or a metal layer
  - a polyester layer \*
  - a cold sealable layer \*

30 5. A packaging material for snacks and ice-cream is composed of the following layers:

- 35
- a release layer \*
  - a printing layer
  - a metal coating or a metal layer
  - an oriented co-extruded polypropylene layer \*
  - a cold sealable layer \*

6. A packaging material for chocolate biscuits and wafers is composed of the following layers:

- 5
  - a polyester layer
  - a printing layer
  - an adhesive layer \*
  - a metal coating or a metal layer
  - a PVDC coating layer \*
- 10
  - an oriented polypropylene layer \*
  - an acrylic coating layer \*

7. A packaging material for biscuits is composed of the following layers:

- 15
  - an anti-scratch coating layer \*
  - a printing layer
  - a paper layer (calendered)
  - a metal coating or a metal layer
  - an oriented co-extruded polypropylene layer \*
- 20

8. A packaging material for high-quality biscuits is composed of the following layers:

- 25
  - a polyester layer
  - a printing layer
  - an adhesive layer \*
  - a paper layer (calendered)
  - an adhesive layer \*
- 30
  - a metal coating or a metal layer
  - an oriented co-extruded polypropylene layer \*

9. A packaging material for detergents is composed of the following layers:

- 35
  - a polyester layer \*
  - a printing layer

- an adhesive layer \*
- a polyethylene layer \*

5 10. A packaging material for ham and cheese is composed of the following layers (the product is between the upper and lower layer):

The upper layer:

- 10
- a polyester layer with a PVDC coating as an outer surface
  - a printing layer
  - an adhesive layer \*
  - a polyethylene layer

The lower layer:

15

- a polyethylene layer \*
- an adhesive layer
- a polyamide layer \*

20

11. A packaging material for coffee and milk powder is composed of the following layers:

- 25
- a polyester layer
  - a printing layer
  - an adhesive layer \*
  - a polyethylene layer
  - a metal coating or a metal layer
  - an adhesive layer \*
  - a polyethylene layer \*
- 30

12. A packaging material for nuts and dry fruits is composed of the following layers:

- 35
- an acrylic coating layer \*
  - a polypropylene layer
  - a PVOH coating layer \*

- a printing layer
- an adhesive layer \*
- a white polyethylene layer \*

5 13. A peelable packaging material for example for lids of yogurt cans is composed of the following layers:

- 10
- a polyester layer \*
  - a printing layer
  - an adhesive layer \*
  - a polyester layer \*
  - a layer of peelable material \*

Claims:

5 1. A method for forming a film on a planar surface, **characterized** in that a granular layer is applied on the planar surface by using electrostatic forces, and the granular layer is finished to form the film.

10 2. The method according to claim 1, **characterized** in that the planar surface is a sheet-like substrate which is allowed to travel as a continuous web between electrodes which are located at opposite sides of the web and are in different potentials, and particles which are to form the granular layer are charged and applied on the web by utilizing an electric field created by the electrodes.

15 3. The method according to claim 2, **characterized** in that the electrodes at the opposite sides of the web are a pair comprising either a positive electrode and a negative electrode, or a negative or a positive electrode and an earthing electrode.

20 4. The method according to any preceding claim, **characterized** in that the substrate comprising the granular layer is finished by using heat and pressure.

25 5. The method according to claim 4, **characterized** in that the substrate is finished in a calender.

6. The method according to claim 2, **characterized** in that the particles are carried to the web in a gaseous flow.

30 7. The method according to claim 1, **characterized** in that the electrostatic forces are created by corona charging electrodes.

35 8. The method according to claim 1, **characterized** in that the electrostatic forces are created by a system producing triboelectric charges.



9. The method according to claim 1, **characterized** in that the electrostatic forces are created by using both corona charging electrodes and a system producing triboelectric charges.

5 10. The method according to claim 1, **characterized** in that the planar surface is a counter surface on which the granular layer is applied, the granular layer is finished to form the film, and the film is peeled off from the counter surface.

10 11. A device for forming a film on a planar surface, **characterized** in that it comprises

- means for charging and applying a powdery film forming material on the planar surface as a granular layer, and
- means for finishing the granular layer.

15

12. The device according to claim 11, **characterized** in that means for charging and applying the powdery film forming material on the planar surface as a granular layer comprises corona charging electrodes.

20 13. The device according to claim 11, **characterized** in that means for charging and applying the powdery film forming material on the planar surface as a granular layer comprises a system producing triboelectric charges.

25 14. The device according to any preceding claim 11 - 13, **characterized** in that means for charging and applying the powdery film forming material on the planar surface as a granular layer comprises a source of a gaseous medium.

30 15. The device according to any preceding claim 11 - 14, **characterized** in that means for finishing the granular layer comprises a calender with at least one heated roll.

35 16. A method in rebuilding a converting line comprising means for forming a film on a surface of a sheet-like substrate, **characterized** in that the existing means for forming the film on the surface of the sheet-like substrate are replaced by a device comprising means for charging

and applying a powdery film forming material on the substrate as a granular layer, and means for finishing the granular layer.

5 17. A multilayer sheet-like product comprising a film layer, **characterized** in that the film layer has been formed by applying a granular layer on the surface of the substrate by using electrostatic forces, and the granular layer has been finished to form the film.

10 18. The product according to claim 17, **characterized** in that product includes a metal coated layer or a metal layer.

15 19. The product according to claim 17 or 18, **characterized** in that the oxygen transmission rate of the product is at the most 180 ml/m<sup>2</sup>/24 h (23°C, RH 0 %).

20. The product according to any preceding claim 17 - 19, **characterized** in that the water vapour transmission rate of the product is at the most 2,5 g/m<sup>2</sup>/24 h.

**(57) Abstract:**

The present invention relates to a method for forming a film on a planar surface. In the method, a granular layer is applied on the planar surface by using electrostatic forces, and the granular layer is finished to form the film. The present invention also relates to a device for forming a film on a planar surface, a method in rebuilding a converting line comprising means for forming a film on a surface of a sheet-like substrate and a multilayer sheet-like product comprising a film layer.

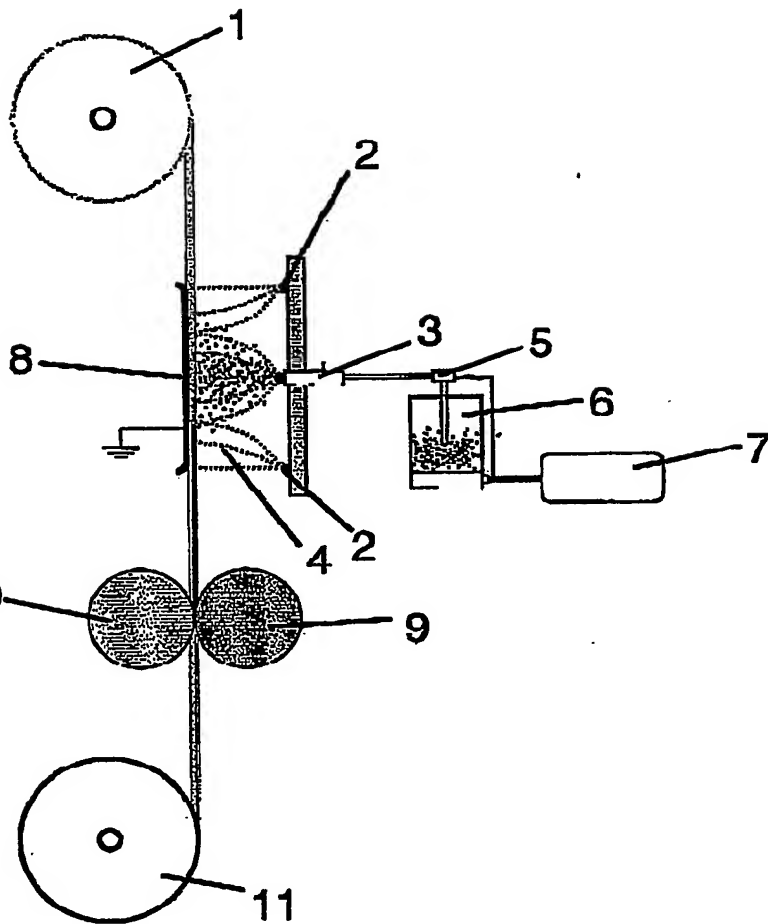


Fig.